

UNIVERSIDAD DE CANTABRIA
DEPARTAMENTO DE INGENIERÍA DE COMUNICACIONES



TESIS DOCTORAL

**Amplificadores de Banda Ancha y Bajo Ruido Basados
en Tecnología de GaAs para Aplicaciones de
Radiometría**

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Publicaciones relacionadas con la Tesis

Revistas Internacionales

1. B. Aja, M.L de la Fuente, J.P. Pascual, M. Detratti, E. Artal., "GaAs PHEMT Broadband Low Noise Amplifier for Millimeter Wave Radiometer", *Microwave and Optical Technology Letters (Wiley Periodicals, Inc)*, Vol. 39, Issue 6, pp. 475-479, Dec. 2003
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Anexo A

Esquemas de una Rama de los Módulos Posteriores del Radiómetro Planck

A.1. Introducción

A continuación se muestran los esquemas para cada una de las ramas de los módulos posteriores (BEM) a 30 y 44 GHz. Se indican los componentes utilizados en los diseños. Algunos de estos componentes cambian en las unidades de los BEM de calificación o de vuelo.

A.2. Rama del Módulo Posterior de 30 GHz

El esquema de una rama del BEM a 30 GHz se muestra en la Figura A.1. En cada rama, el LNA consta de dos amplificadores de bajo ruido en cascada, con el fin de obtener la ganancia necesaria. A continuación se encuentra el filtro microstrip paso banda, el detector cuadrático y por último el amplificador de continua.

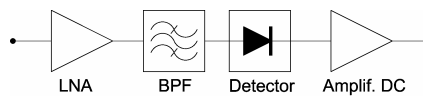


Figura A.1. Esquema de una rama del módulo posterior a 30 GHz

La Figura A.2 muestra con más detalle cada uno de los subsistemas que forman una rama, con la entrada de RF y la transición como primer elemento, las alimentaciones de +5 V y -5 V y la salida equilibrada del amplificador de continua.

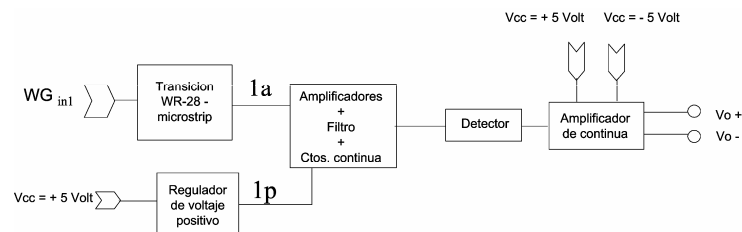


Figura A.2. Esquema de una rama en el BEM de 30 GHz

En los siguientes apartados se detalla el esquema eléctrico y los componentes de los elementos que forman el sistema de la Figura A.2.

A.2.1. Regulador positivo

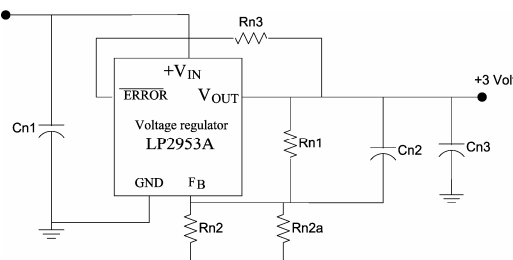


Figura A.3. Regulador de voltaje positivo del BEM de 30 GHz

Tabla A.1. Componentes del regulador positivo del BEM de 30 GHz

Referencia	Descripción	Valor	Referencia	Fabricante
VR1	Regulador	---	LP2953A	National Semiconductor
Rn1	Resistencia	18.7 k Ω	M55342K02B18E7R	Vishay Sfernice
Rn2	Resistencia	23.7 k Ω	M55342K02B23E7R	Vishay Sfernice
Rn2a	Resistencia	28.7 k Ω	M55342K02B28E7R	Vishay Sfernice
Rn3	Resistencia	100 k Ω	M55342K02B100ER	Vishay Sfernice
Cn1	Capacidad	1 μ F	CWR09NB105KBBB	AVX
Cn2	Capacidad	0.1 μ F	CWR09NB104KBBB	AVX
Cn3	Capacidad	6.8 μ F	CWR09MB685KBBB	AVX

A.2.2. RF y circuitos de protección

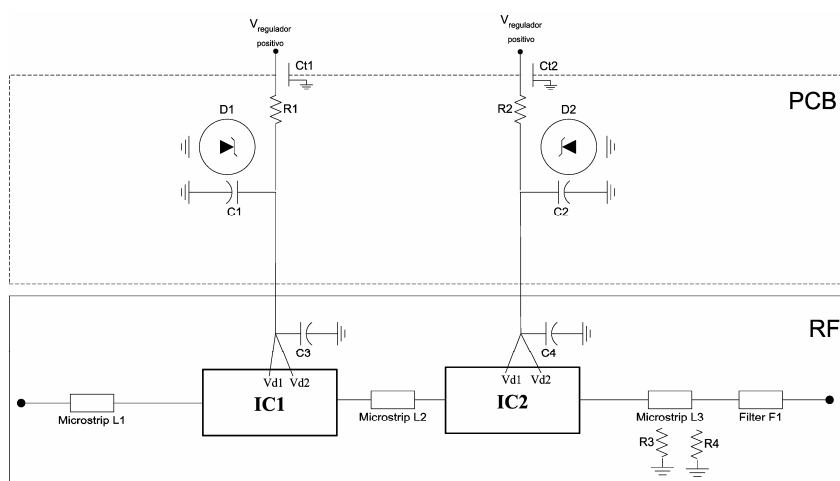


Figura A.4. RF con Amplificadores + Filtro + circuitos de polarización y de protección de continua del BEM de 30 GHz

En la caja de este montaje van dos condensadores pasamuros (Ct1, Ct2), como se muestra en la Figura 6.34.

Los hilos de oro utilizados para las conexiones de los circuitos integrados, líneas y condensadores en la parte de RF son de diámetro 17.5 μ m, y en estas conexiones se utiliza un sólo hilo de oro. Para la equalización se utilizan dos hilos de oro que unen las resistencias R3 y R4 a la línea microstrip L3. Para unir el filtro de Duroid, se pega cinta de oro (de grosor 25 μ m y anchura 0.254 mm) con epoxy sobre el filtro y se une mediante varios hilos de oro soldado a la línea L3 de 50 Ohm en alúmina. Una fotografía de este montaje se muestra en la Figura 6.32.

La transición de guía de onda a microstrip en la entrada se une a la línea, L1, de 50 Ohm en Alúmina con un trozo de cinta de oro (de grosor 25 μm y anchura 0.254 mm), que se pega en ambos lados con epoxy. La pasta conductora de epoxy utilizada en todos los casos es la E3081 de Epotek.

Tabla A. 2. Componentes la red de protección del BEM de 30 GHz

Referencia	Descripción	Valor	Referencia	Fabricante
R1	Resistencia	10 Ω	M55342K02B10D0R	Vishay Sfernice
R2	Resistencia	10 Ω	M55342K02B10D0R	Vishay Sfernice
D1	Zener	$V_z=4.3$ V	1N4623UR-1	CDI
D2	Zener	$V_z=4.3$ V	1N4623UR-1	CDI
C1	Capacidad	0.1 μF	CWR09NB104KBBB	AVX
C2	Capacidad	0.1 μF	CWR09NB104KBBB	AVX
Ct1	Capacidad	33 nF	FC030-3-333-SV-25HT	Eurofarad
Ct2	Capacidad	33 nF	FC030-3-333-SV-25HT	Eurofarad

Tabla A.3. Componentes la parte de RF del BEM de 30 GHz

Referencia	Descripción	Valor	Referencia	Fabricante
C3	Capacidad	100 pF	DICAP D20BU101M5PB	DILABS/USA
C4	Capacidad	100 pF	DICAP D20BU101M5PB	DILABS/USA
IC1	MMIC-LNA	---	HMC263	Hittite
IC2	MMIC-LNA	---	HMC263	Hittite
R3	Resistencia	1 k Ω	S0302AP102JG	SOTA
R4	Resistencia	1 k Ω	S0302AP102JG	SOTA
L1	Línea microstrip	50 $\Omega @ 30\text{GHz}$	Alumina	Reinhardt Microtech
L2	Línea microstrip	50 $\Omega @ 30\text{GHz}$	Alúmina	Reinhardt Microtech
L3	Línea microstrip	50 $\Omega @ 30\text{GHz}$	Alúmina	Reinhardt Microtech
F1	Filtro paso banda	μstrip Coupled lines	F30 D2 20 (Duroid 6002)	Rogers Corporation

A.2.3. Detector

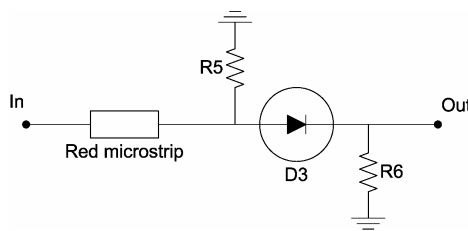


Figura A.5. Detector del BEM de 30 GHz

Tabla A.4. Componentes del detector del BEM de 30 GHz

Referencia	Descripción	Valor	Referencia	Fabricante
D3	Diodo GaAs	---	HSCH 9161	Agilent Technologies
R5	Resistencia	100 Ω	S0302EP101JG	SOTA
R6	Resistencia	100 k Ω	M55342K02B100ER	Vishay Sfernice

A.2.4. Amplificador de continua

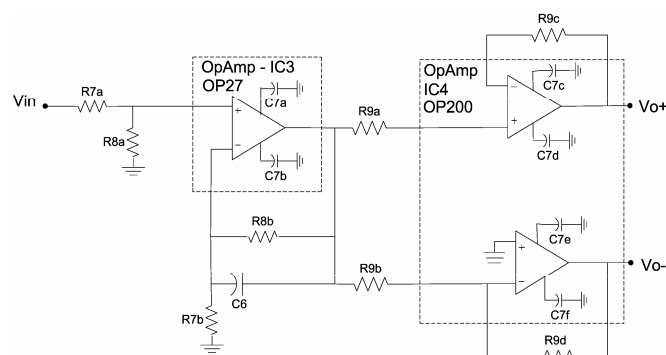


Figura A.6. Amplificador de continua

Tabla A.5. Componentes del amplificador de continua del BEM de 30 GHz

Referencia	Descripción	Valor	Referencia	Fabricante
IC3	Amplificador operacional	---	OP27AJ	Burr-Brown
IC4 (a,b)	Amplificador operacional	---	OP200A	Analog Devices
R7 a (R1)	Resistencia	51 k Ω	M55342K02B51ER	Vishay Sfernice
R7 b (R3)	Resistencia	100 Ω	M55342K02B100DR	Vishay Sfernice
R8 a (R2)	Resistencia	51 k Ω	M55342K02B51ER	Vishay Sfernice
R8 b (R4)	Resistencia	39 k Ω	M55342K02B39ER	Vishay Sfernice
R9 (a,b,c,d) (R5)	Resistencia	10 k Ω	M55342K02B10ER	Vishay Sfernice
C6	Capacidad	47 pF	CDR01BP470BJNM	AVX
C7 (a,b,c,d,e,f)	Capacidad	33 nF	CDR32BX333AJNM	AVX

A.3. Módulo Posterior de 44 GHz

El esquema de una rama del BEM a 44 GHz se muestra en la Figura A.7. En cada rama, el LNA consta de dos amplificadores de bajo ruido y atenuadores microstrip en cascada. A continuación se encuentra el filtro microstrip paso banda, el detector cuadrático y por último el amplificador de continua.

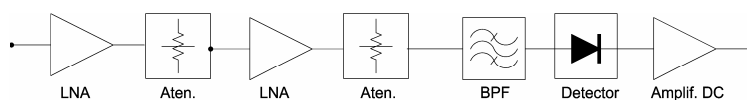


Figura A.7. Esquema de una rama del módulo posterior a 44 GHz

La Figura A.8 muestra con más detalle cada uno de los subsistemas que forman una rama, con la entrada de RF y la transición como primer elemento, las alimentaciones de +5 V y -5 V y la salida equilibrada del amplificador de continua.

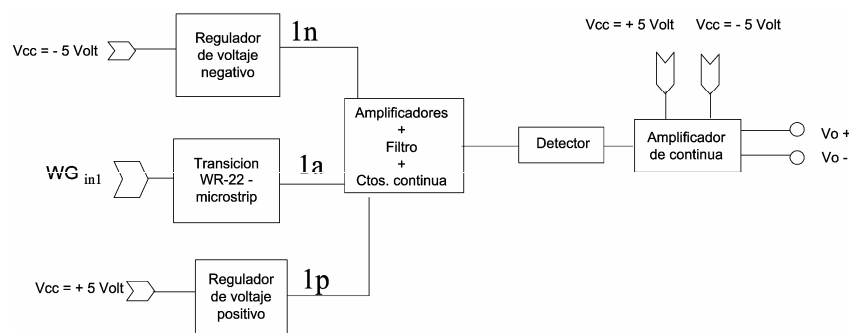


Figura A.8. Esquema de una rama en el BEM de 44 GHz

En los siguientes apartados se detalla el esquema eléctrico y los componentes de los elementos que forman el sistema de la Figura A.8.

A.3.1. Regulador positivo

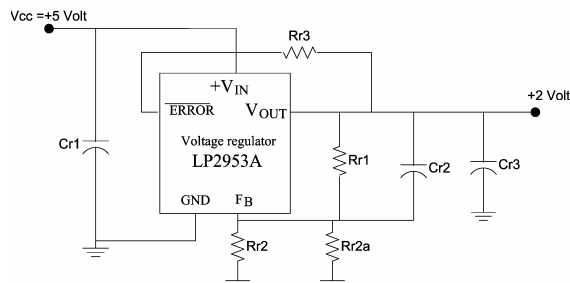


Figura A.9. Regulador de voltaje positivo del BEM de 44 GHz

Tabla A.6. Componentes del regulador positivo del BEM de 44 GHz

Referencia	Descripción	Valor	Referencia	Fabricante
VR1	Regulador	---	LP2953A	National Semiconductors
Rr1	Resistencia	7k5 Ω	M55342K02B7E5R	Vishay Sfernice
Rr2	Resistencia	23.7 k Ω	M55342K02B23E7R	Vishay Sfernice
Rr2a	Resistencia	23.7 k Ω	M55342K02B23E7R	Vishay Sfernice
Rr3	Resistencia	100 k Ω	M55342K02B100ER	Vishay Sfernice
Cr1	Capacidad	1 μ F	CWR09NB105KBBB	AVX
Cr2	Capacidad	0.1 μ F	CWR09NB104KBBB	AVX
Cr3	Capacidad	6.8 μ F	CWR09MB685KBBB	AVX

A.3.2. Regulador negativo

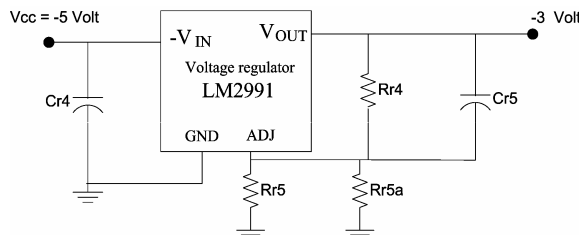


Figura A.10. Regulador de voltaje negativo del BEM de 44 GHz

Tabla A.7. Componentes del regulador negativo del BEM de 44 GHz

Referencia	Descripción	Valor	Referencia	Fabricante
VR2	Regulador	---	LM2991	National Semiconductors
Rr4	Resistencia	3320 Ω	M55342K02B3E32R	Vishay Sfernice
Rr5	Resistencia	4400 Ω	M55342K02B4E4R	Vishay Sfernice
Rr5a	Resistencia	4400 Ω	M55342K02B4E4R	Vishay Sfernice
Cr4	Capacidad	1 μ F	CWR09NB105KBBB	AVX
Cr5	Capacidad	1 μ F	CWR09NB105KBBB	AVX

A.3.3. Parte de RF y circuitos de polarización y protección

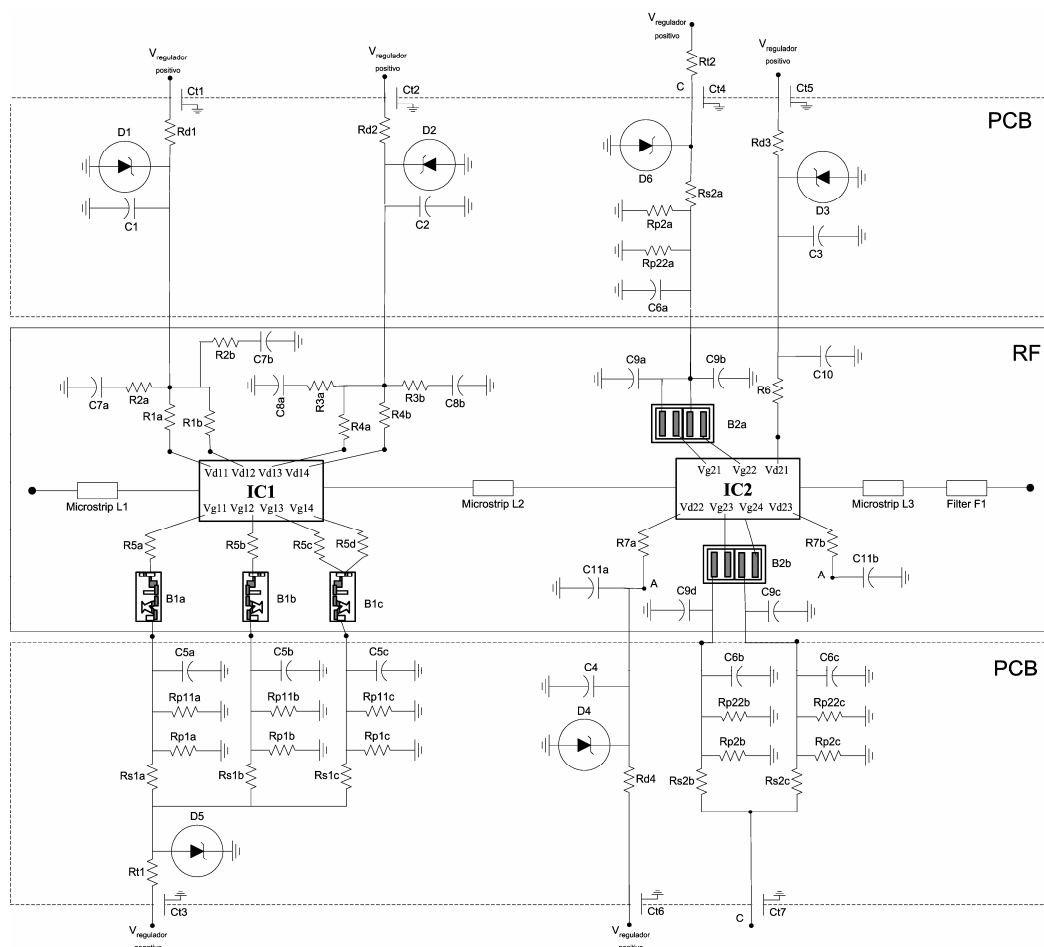


Figura A.11. Amplificadores de RF, filtro y circuitos de polarización y de protección de continua del BEM de 44 GHz

En la caja de este montaje van siete pasamuros como se muestra en la Figura 6.76. Tres pasamuros son para la polarización del primer MMIC (IC1), dos de los drenadores y uno de todas las puertas. Los otros cuatro pasamuros son para la polarización del segundo MMIC (IC2), dos de las puertas y dos de los drenadores.

Al igual que en los prototipos de 30 GHz, los hilos de oro utilizados para las conexiones de los circuitos integrados, líneas y condensadores en la parte de RF son de diámetro 17.5 μ m, y en estas conexiones se utiliza un sólo hilo de oro. Para unir el filtro de Duroid F1, se pega cinta de oro (de grosor 25 μ m y anchura 0.254 mm) con epoxy sobre el filtro y se une mediante varios hilos de oro soldado a la línea L3 de 50 Ohm en alúmina. Una fotografía de este montaje se muestra en la Figura 6.75.

La transición de guía de onda a microstrip en la entrada se une a la línea de 50 Ohm en alúmina con un trozo de cinta de oro (de grosor 25 m y de anchura 0.254 mm), y se pega en ambos lados con epoxy. La pasta conductora de epoxy utilizada en todos los casos es la E3081 de Eptek.

Tabla A.8. Componentes de polarización y protección del BEM de 44 GHz

Referencia	Descripción	Valor	Referencia	Fabricante
Rd1	Resistencia	10 Ω	M55342K02B10D0R	Vishay Sfernice
D1	Zener	$V_z = 2.2$ V	1N4616UR-1	CDI
C1	Capacidad	0.1 μ F	CWR09NB104KBBB	AVX
Rd2	Resistencia	75 Ω	M55342K02B75DR	Vishay Sfernice
D2	Zener	$V_z = 2.2$ V	1N4616UR-1	CDI
C2	Capacidad	0.1 μ F	CWR09NB104KBBB	AVX
Rd3	Resistencia	10 Ω	M55342K02B10DR	Vishay Sfernice
D3	Zener	$V_z = 2.2$ V	1N4616UR-1	CDI
C3	Capacidad	0.1 μ F	CWR09NB104KBBB	AVX
Rd4	Resistencia	10 Ω	M55342K02B10DR	Vishay Sfernice
D4	Zener	$V_z = 2.2$ V	1N4616UR-1	CDI
C4	Capacidad	0.1 μ F	CWR09NB104KBBB	AVX
Rt1	Resistencia	61.9 k Ω	M55342K02B61E9R	Vishay Sfernice
D5	Zener	$V_z = 2.2$ V	1N4616UR-1	CDI
Rs1 (a,b,c)	Resistencia	23.7 k Ω	M55342K02B23E7R	Vishay Sfernice
Rp1 (a,b,c)	Resistencia	11.5 k Ω	M55342K02B11E5R	Vishay Sfernice
Rp11 (a,b,c)	Resistencia	100 k Ω	M55342K02B100ER	Vishay Sfernice
C5 (a,b,c)	Capacidad	0.1 μ F	CWR09NB104KBBB	AVX
Rt2	Resistencia	23.7 k Ω	M55342K02B23E7R	Vishay Sfernice
D6	Zener	$V_z = 2.2$ V	1N4616UR-1	CDI
Rs2 (a,b,c)	Resistencia	21.5 k Ω	M55342K02B21E5R	Vishay Sfernice
Rp2 (a,b,c)	Resistencia	53.6 k Ω	M55342K02B53E6R	Vishay Sfernice
Rp22 (a,b,c)	Resistencia	100 k Ω	M55342K02B100ER	Vishay Sfernice
C6 (a,b,c)	Capacidad	0.1 μ F	CWR09NB104KBBB	AVX
Ct1	Capacidad	33 nF	FC030-3-333-SV-25HT	Eurofarad
Ct2	Capacidad	33 nF	FC030-3-333-SV-25HT	Eurofarad
Ct3	Capacidad	33 nF	FC030-3-333-SV-25HT	Eurofarad
Ct4	Capacidad	33 nF	FC030-3-333-SV-25HT	Eurofarad
Ct5	Capacidad	33 nF	FC030-3-333-SV-25HT	Eurofarad
Ct6	Capacidad	33 nF	FC030-3-333-SV-25HT	Eurofarad
Ct7	Capacidad	33 nF	FC030-3-333-SV-25HT	Eurofarad

Tabla A.9. Componentes de la parte de RF y de polarización del BEM de 44 GHz

Referencia	Descripción	Valor	Referencia	Fabricante
L1	Línea microstrip	50 Ω @ 44GHz		Reinhardt Microtech
L2	Atenuador microstrip	3/5 dB	BE44-1212/BE44-1222	Thin Film Products
L3	Atenuador microstrip	3/13 dB	BE44-1213/BE44-1223	Thin Film Products
F1	Filtro paso banda	μ strip Coupled lines	F44_3E_A20_2 (Duroid 6002)	Rogers Corporation
IC1	MMIC-LNA	---	mc_lna44 (P20H20_2C4)	OMMIC
IC2	MMIC-LNA	---	Lf_lna443v (P20H1_2H1)	OMMIC
R2 (a,b)	Resistencia	100 Ω	S0302 P101JG	SOTA/USA
C7 (a,b)	Capacidad	22 pF	DICAP D15BH220M5PB	DILABS/USA
R1 (a,b)	Resistencia	10 Ω	S0302 AP100JG	SOTA/USA
R3 (a,b)	Resistencia	100 Ω	S0302 P101JG	SOTA/USA
C8 (a,b)	Capacidad	22 pF	DICAP D15BH220M5PB	DILABS/USA
R4 (a,b)	Resistencia	10 Ω	S0302 AP100JG	SOTA/USA
B1 (a,b,c)	Bias Filter Network	---	B28BHFBN01	DILABS/USA
R5 (a,b,c,d)	Resistencia	100 Ω	S0302 AP101JG	SOTA/USA

C9 (a,b,c,d)	Condensador	100 pF	DICAP D20BU101M5PB	DILABS/USA
B2 (a,b)	RF Blocking Network	---	J30BHBA02LX2	DILABS/USA
C10	Condensador	100 pF	DICAP D20BU101M5PB	DILABS/USA
R6	Resistencia	10 Ω	S0302 AP100JG	SOTA/USA
C11 (a,b)	Condensador	100 pF	DICAP D20BU101M5PB	DILABS/USA
R7 (a,b)	Resistencia	10 Ω	S0302 AP100JG	SOTA/USA

A.3.4. Detector

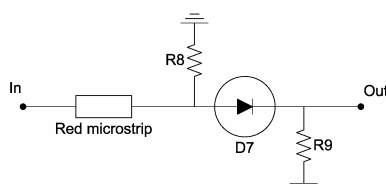


Figura A.12. Detector del BEM de 44 GHz

Tabla A.10. Componentes del detector del BEM de 44 GHz

Referencia	Descripción	Valor	Referencia	Fabricante
D7	Diodo GaAs	---	HSCH 9161	Agilent Technologies
R8	Resistencia	100 Ω	S0302EP101JG	SOTA
R9	Resistencia	100 k Ω	M55342K02B100ER	Vishay Sfernice

A.3.5. Amplificador de continua

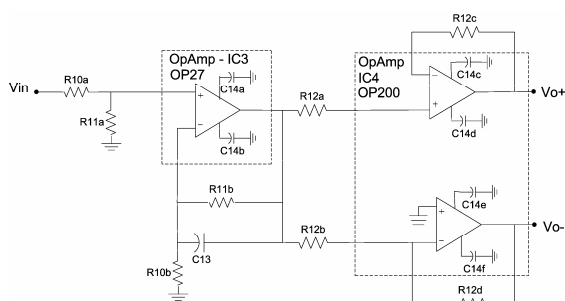


Figura A.13. Amplificador de continua del BEM de 44 GHz

Tabla A.11. Componentes del amplificador de continua del BEM de 44 GHz

Referencia	Descripción	Valor	Referencia	Fabricante
IC3	Amplificador operacional	---	OP27AJ	Burr-Brown
IC4 (a,b)	Amplificador operacional	---	OP200A	Analog Devices
R10a (R1)	Resistencia	100 Ω	M55342K02B100DR	Vishay Sfernice
R10b (R3)	Resistencia	100 Ω	M55342K02B100DR	Vishay Sfernice
R11a (R2)	Resistencia	51 kΩ	M55342K02B51ER	Vishay Sfernice
R11b (R4)	Resistencia	3.6 kΩ	M55342K02B3E6R	Vishay Sfernice
R12 (a,b,c,d) (R5)	Resistencia	10 kΩ	M55342K02B10ER	Vishay Sfernice
C13 (C1)	Capacidad	47 pF	CDR01BP470BJNM	AVX
C14 (a,b,c,d,e,f) (C)	Capacidad	33 nF	CDR32BX333AJNM	AVX

A.3.6. Atenuadores microstrip

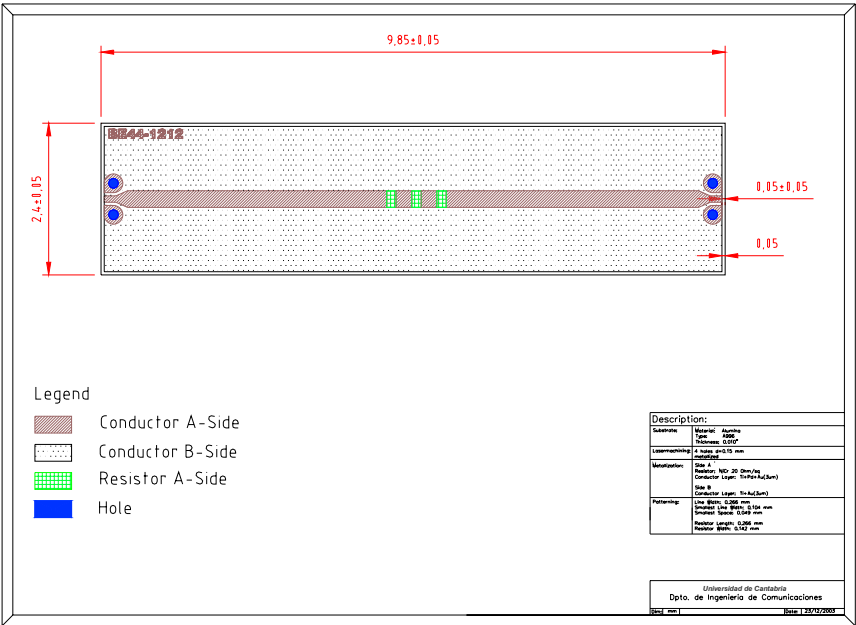


Figura A.14. Atenuador 3 dB en Alumina ($l = 9.9$ mm) con transiciones coplanar microstrip

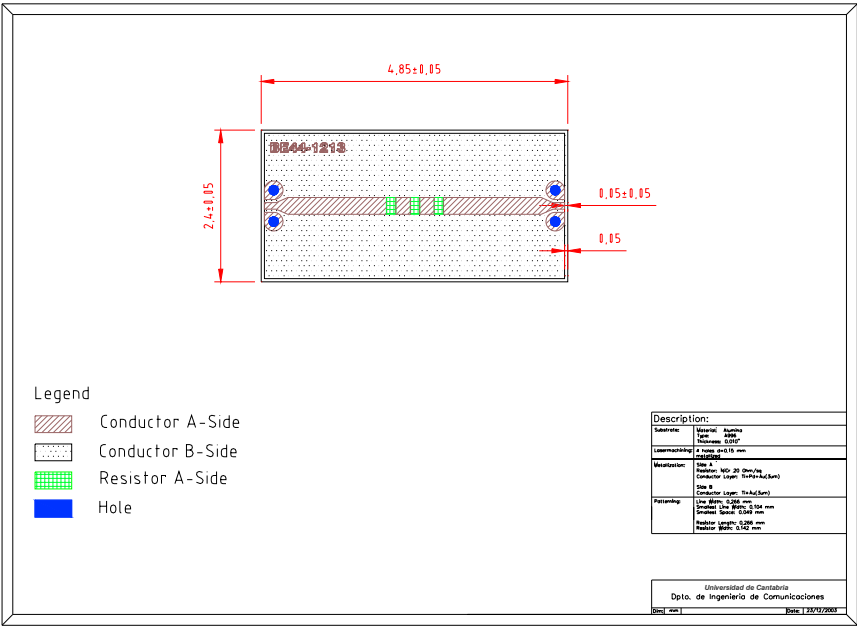


Figura A.15. Atenuador 3 dB en Alumina ($l = 4.9$ mm) con transiciones coplanar microstrip

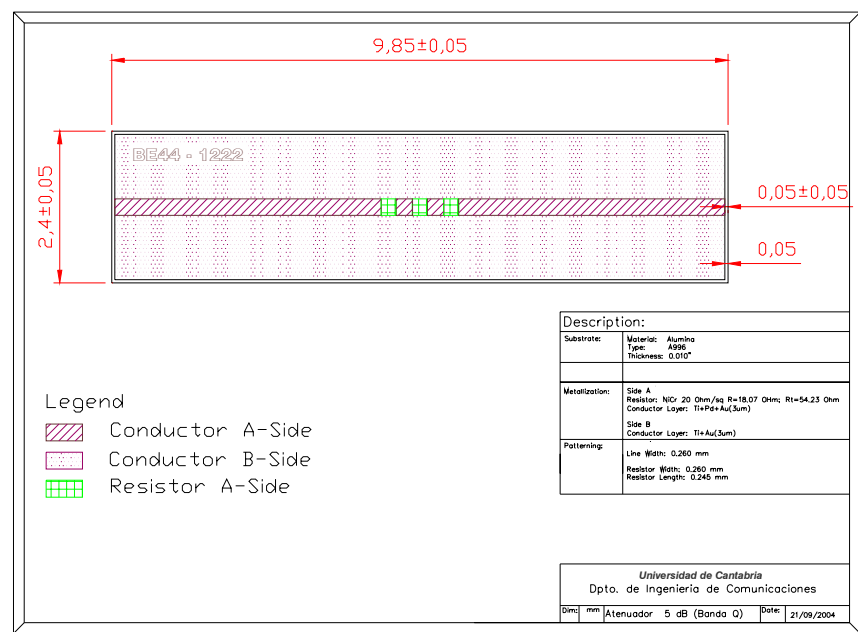


Figura A.16. Atenuador 5 dB en Alumina (l = 9.9 mm) con transiciones coplanar microstrip

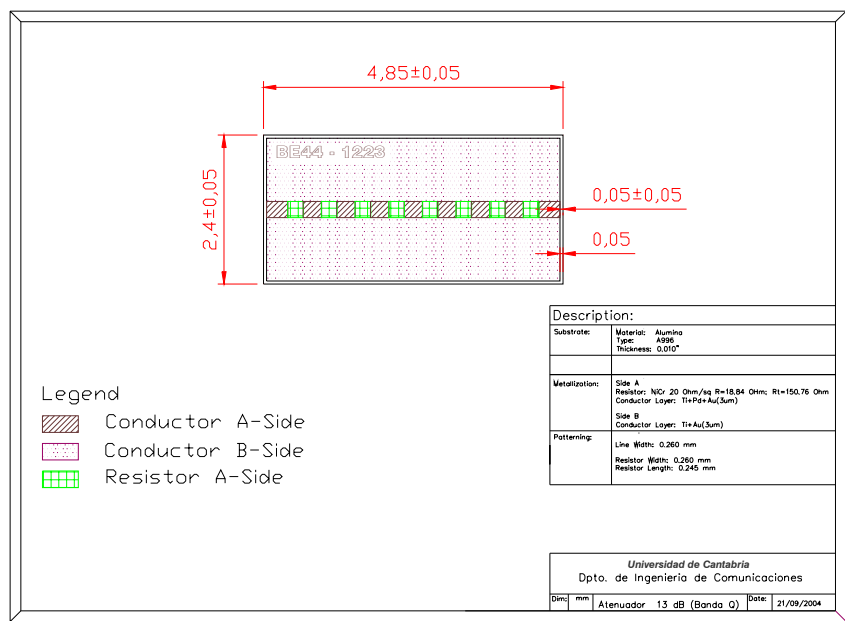


Figura A.17. Atenuador 13 dB en Alumina (l = 4.9 mm) con transiciones coplanar microstrip

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