

1 **Modeling of the binodal curve of ionic liquid/salt aqueous** 2 **systems**

3
4 Enrique Alvarez-Guerra,^a Sónia P.M. Ventura,^b Manuel Alvarez-Guerra,^{*,a}
5 João A.P. Coutinho,^b Angel Irabien^a

6 ^a *Departamento de Ingenierías Química y Biomolecular, Universidad de Cantabria. Avenida de*
7 *los Castros s/n, 39005 Santander, Cantabria, Spain*

8 ^b *Departamento de Química, CICECO, Universidade de Aveiro, 3810-193 Aveiro, Portugal*

9 *Correspondence author: Tel.: +34 942 20 67 77; fax: +34 942 20 15 91. E-mail address:
10 alvarezgm@unican.es (M. Alvarez-Guerra).

11 12 **Abstract**

13 Ionic Liquid-based Aqueous Two Phase Systems (ILATPS) are an innovative technique
14 to separate biomolecules that combines the advantages of liquid-liquid extraction and
15 hydrophilic ionic liquids. Most ILATPS are based on ionic liquids and conventional
16 inorganic salts, and the phase envelope, described by the binodal curve, is usually
17 modeled by empirical equations that are used to determine the phase compositions and
18 assess the ionic liquid recyclability. However, these empirical equations may provide a
19 poor extrapolation ability or low accuracy at the extreme regions of the binodal curve or
20 suffer from problems of convergence. Therefore, the aim of this work is the analysis of
21 the binodal curve equations, comparing the models reported in the literature to describe
22 ILATPS and proposing alternative equations to improve accuracy or to reduce the
23 mathematical complexity. For this purpose, a database compiling binodal experimental

24 data of 100 ILATPS has been built, so that the analysis could make it possible to obtain
25 representative conclusions for all these systems. Several models were developed, and
26 different statistical criteria were used to assess the advantages and disadvantages of each
27 one of these models for the binodal curve. The results show that, when accuracy is
28 critical, a proposed model with just an additional parameter reduced more than 25 % the
29 residual mean squared error (RMSE) with respect to the commonly used equation,
30 without losing the statistical significance of the parameters. For complex problems
31 where an explicit equation in both the concentration of ionic liquid and of salt is needed,
32 the use of an explicit model developed with 3 adjusted parameters that kept high
33 accuracy ($R^2 > 0.996$ and $RMSE < 0.66$) is proposed. Finally, the analysis also revealed
34 that a fitting method based on the minimization of relative errors is recommended to
35 increase the accuracy of the binodal curve at high salt concentrations, which is the
36 crucial region for assessing the recyclability of the ionic liquid.

37

38 **Keywords:** aqueous biphasic system; binodal curve; model; accuracy; ionic liquid recyclability

39

40 1. INTRODUCTION

41 The separation and purification of biomolecules usually represents about 60–90 % of
42 the cost of the final product(s), so downstream processing determines the efficiency and
43 viability of the biotechnological processes [1]. Among the multiple alternatives to
44 separate biomolecules, Ionic Liquid-based Aqueous Two-Phase Systems (ILATPS)
45 stand out for being an innovative technique that combines the advantages of liquid-
46 liquid extraction and ionic liquids [2,3]. ILATPS are powerful alternatives extracting
47 biomolecules and have been widely used in the separation, concentration, and
48 purification of proteins, amino-acids, antibiotics, antioxidants, alkaloids [4-6], among

49 others [2]. They are based on ionic liquids and salts, which form two aqueous phases: an
50 ionic liquid-rich and a salt-rich phase. Many works can be found in literature in which
51 these systems are characterized in terms of the binodal curve, which also makes it
52 possible to compare the various systems with each other to derive information about the
53 mechanisms responsible for the phase separation and the design of novel ATPS.
54 Moreover, an accurate binodal curve is essential to experimentally determine the tie
55 lines by means of the gravimetric method and, in this way, the composition of the two
56 liquid phases [7-9].

57 However, rigorous models of the binodal curve for ILATPS with a theoretical support
58 are not available. In this way, the binodal curve of ILATPS is usually described by
59 means of the empirical equation proposed by Merchuk and collaborators [2,10,11]:

$$60 \quad [IL] = A \exp(B[S]^{0.5} - C[S]^3) \quad (1)$$

61 where [IL] and [S] are the mass fractions of ionic liquid and salt expressed as
62 percentage, respectively, and A , B and C are adjusted parameters. It should be noted that
63 Merchuk's equation was originally proposed to describe conventional aqueous two-
64 phase systems based on polymers and salts. However, this equation also provides
65 relatively high values of the R^2 when modeling ILATPS, but it requires 5 parameters (2
66 fixed and 3 adjusted) to fit the experimental data and some limitations have been
67 detected for this model. In this sense, a higher accuracy may be required for describing
68 the extreme regions of the binodal curve (at very high ionic liquid or salt
69 concentrations) [7,12]. The region of very high salt mass fractions is essential to assess
70 the ionic liquid recyclability to the process, so the accuracy of the binodal curve in this
71 region is particularly important [13]. In addition, Eq. 1 may cause problems of
72 convergence when it is used in the resolution of more complex problems (recyclability
73 experimental schemes, for example) due to the fact that it is clearly non-linear and

74 implicit in salt concentration [14]. Therefore, the development of alternative models of
 75 the binodal curve that overcome these drawbacks is particularly interesting. In the
 76 literature, other empirical expressions have been proposed as alternative models to
 77 enhance the accuracy [15-17]:

$$78 \quad [IL] = \exp(a + b[S]^{0.5} + c[S] + d[S]^2) \quad (2)$$

$$79 \quad [IL] = a_1 \exp\left(-\frac{[S]}{b_1}\right) + a_2 \exp\left(-\frac{[S]}{b_2}\right) + c \quad (3)$$

80 where a , a_1 , a_2 , b , b_1 , b_2 and c are adjusted parameters. Both equations 2 and 3 contain a
 81 higher number of adjusted parameters (4 and 5, respectively) than Merchuk's equation.
 82 Another approach reported in previous works [15,17-19] implies a binodal curve model
 83 based on statistical geometry methods, developed by Guan et al. [20] for aqueous
 84 polymer-polymer systems. This binodal equation has a theoretical support by means of
 85 the concept of effective excluded volume (EEV) and contains only two adjusted
 86 parameters:

$$87 \quad \ln\left(V_{213}^* \frac{[S]}{M_S} + f_{213}\right) + V_{213}^* \frac{[IL]}{M_{IL}} = 0 \quad (4)$$

88 where V_{213}^* is the scaled EEV of salt; f_{213} is the volume fraction of unfilled effective
 89 available volume after tight packing of the salt molecules into the ionic liquid molecules
 90 network in ionic liquid aqueous solutions; and M_S and M_{IL} are the molecular masses of
 91 the salt and the ionic liquid, respectively. It should be highlighted that only this binodal
 92 curve model has some theoretical foundation, in contrast with the remaining models,
 93 which are purely empirical. Few studies have carried out a comparison among models
 94 for the binodal curve [15,17,21]. Nevertheless, these analyses have been done using a
 95 reduced number of systems (lower than 10 in all the cases) and very simple statistical
 96 criteria, such as the standard deviation and/or the R^2 coefficient. As a result, the

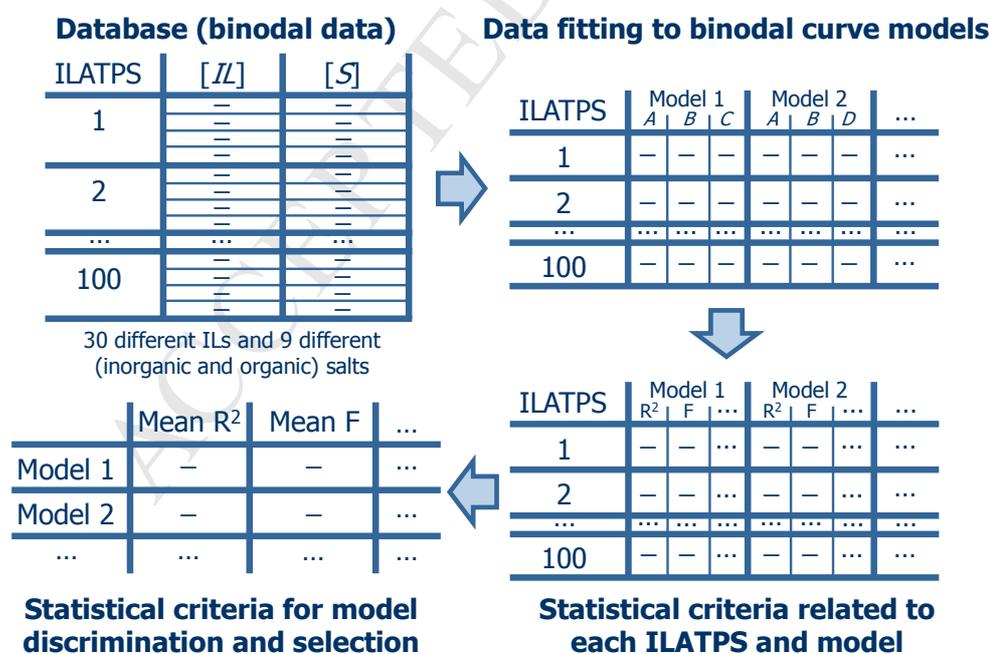
97 conclusions derived from these works with respect to the selection of the binodal curve
 98 model cannot be easily extrapolated to the hundreds of ILATPS described in literature.
 99 In this way, the aim of this work is the analysis of the binodal curve equation to
 100 describe ILATPS based on ionic liquids and salts, comparing the previous models and
 101 proposing either alternative equations which may improve its accuracy or simpler the
 102 mathematical models that keep successful performances. For this purpose, a database
 103 with the binodal data of 100 ILATPS was built and subsequently analyzed so that the
 104 conclusions obtained are representative for all these systems. Furthermore, different
 105 statistical criteria have been used in order to discuss in detail the advantages and
 106 disadvantages of each binodal equation.

107

108 2. METHODS

109 2.1. Methodology

110 The methodology followed in this study is graphically summarized in Fig. 1.



111

112 Fig. 1-Scheme of the methodology followed in this work.

113

114 Binodal data from 100 ILATPS systems were compiled from the literature [7,22-30] in
115 order to assure that the conclusions derived from the study are representative of these
116 types of systems. The database created included 100 ILATPS systems, which involved
117 30 different ILs and 9 different (inorganic and organic) salts. The binodal curves of
118 these ILATPS were determined at room temperature, as liquid-liquid extraction with
119 these systems is usually carried out at this temperature. In addition, it is expected that
120 the conclusions derived in this work from the analysis of the binodal curve of ILATPS
121 at room temperature can also be applied to other temperatures, as the linear dependency
122 of the adjusted parameters of Merchuk's equation with respect to temperature suggests.
123 With respect to the influence of the temperature on ILATPS, the biphasic region
124 decreases with the increase in this variable, which implies that the higher the
125 temperature, the higher the salt and ionic liquid concentrations required for phase
126 separation. However, the intensity of the temperature effect on the phase diagrams
127 depends on the inorganic salt employed [2]. The complete dataset is included in Table
128 S1 as Supplementary Material. For each ILATPS, the binodal data were fitted to each
129 model that was considered in the study, obtaining the values of the adjusted parameters
130 and the statistical criteria that will be described in section 2.2. Finally, for the
131 discrimination and selection of the models, the means of the statistical criteria were
132 calculated, and these means, for the 100 ILATPS, are the values that will be reported in
133 section 3 "Results and discussion".

134

135 **2.2. Statistical criteria for the discrimination and model selection**

136 The discrimination and selection of the binodal curve models has been carried by means
137 of different statistical criteria that consider the accuracy, the significance of the
138 parameters or the number of adjusted parameters [31]:

139 - Coefficient of determination (R^2), which indicates the proportionate amount of
140 variation in the response explained by the independent variable.

141 - The wideness of the confidence interval, which is a measure of the significance of the
142 parameters; if a parameter is significant, it should not contain the zero value.

143 - Fischer's F value (F), which is based on a null hypothesis that advocates for the
144 adequacy of the model to the observed values of the measured variable.

145 - The residual mean squared error (RMSE), which is often considered a measure of the
146 difference of the predicted values of the variable and the experimental observations.

147 - The Akaike information criterion (AIC), which gives information of the goodness of
148 the fit while penalizing model overfitting by increasing the number of parameters of the
149 model.

150 In general, the quality of each model to describe the experimental data increases with
151 the value of R^2 and F, and as the wideness of the confidence interval, the RMSE and the
152 AIC decrease. As previously explained, each model will be assessed by the mean value
153 of these statistical criteria obtained for each of the ILATPS included in the database.
154 However, in the case of the wideness of the confidence interval, as this criterion is
155 determined as the mean of relative wideness (with respect to the value of each
156 parameter) of all the parameters for each ILATPS, to avoid the interference of the
157 extreme values, each model is characterized by the median wideness of the 100 ILATPS
158 instead of by the mean value.

159

160 **3. RESULTS AND DISCUSSION**

161 **3.1. Assessment of the exponents of the Merchuk's equation**

162 As previously stated, Merchuk's equation is widely applied to fit the binodal curve of
163 ILATPS, even though it was developed to conventional polymer-salt APTS models

164 [10]. In this sense, it should be noticed that this equation contains two constant
 165 parameters that correspond to both exponents (see Eq. 1), meaning that the values used
 166 for the polymer-salt ATPS (0.5 and 3.0) may not be the most suitable ones to model
 167 ILATPS. Therefore, alternative values for the exponents of Merchuk's equation were
 168 tested in order to assess if the fitting of the binodal data can be improved. To carry out
 169 this assessment, the binodal data of the 100 ILATPS systems of the database were fitted
 170 using different combinations of values of the Merchuk's equation exponents. The
 171 results of the mean R^2 obtained for each pair of values of the exponents are summarized
 172 in Table 1.

173

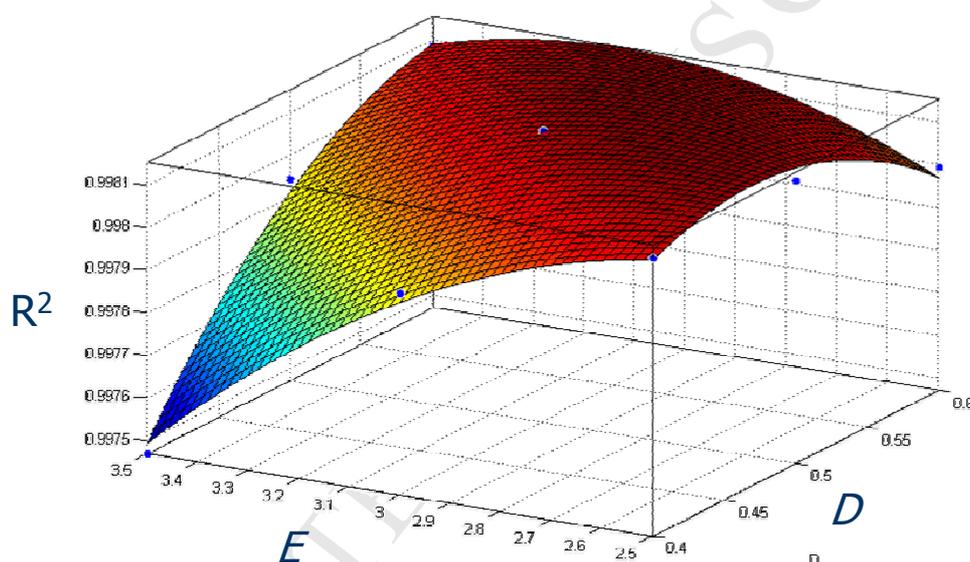
174 Table 1-Mean R^2 obtained in the fitting of the ILATPS of the database of this study
 175 using different values of exponents D and E of Merchuk's equation: $[IL] = A \exp(B$
 176 $[S]^D - C [S]^E)$

| <i>E</i> | <i>D</i> | | |
|------------|------------|----------------|------------|
| | 0.4 | 0.5 | 0.6 |
| 2.5 | 0.99812 | 0.99813 | 0.99799 |
| 3.0 | 0.99794 | 0.99815 | 0.99812 |
| 3.5 | 0.99747 | 0.99794 | 0.99808 |

177

178 The fitting of these mean R^2 values to a quadratic polynomial expression (Fig. 2) shows
 179 how they vary depending on the values of the exponents D and E used. The maximum
 180 value of mean R^2 for the 100 ILATPS was obtained when exponents were $D=0.506$ and
 181 $E=2.74$. Consequently, the binodal data of these systems were fitted using these values
 182 of the exponents, obtaining that this maximum mean R^2 was equal to 0.99817, which
 183 resulted to be very similar to the value of 0.99815 obtained with the original Merchuk's
 184 equation (i.e. $D=0.5$, $E=3.0$, Table 1). As can be seen, there is a region of combinations
 185 (D, E) in which almost the same mean R^2 value is obtained (higher than 0.9981) and
 186 that contains the original values of Merchuk's equation. Since the studies in the

187 literature that model the binodal curve of ILAPTS with Merchuk's equation routinely
 188 use 0.5 and 3.0 as values for the exponents, the very small increase in R^2 obtained does
 189 not justify to propose the change of these exponents. Although the values of the
 190 exponents (0.5, 3.0) are empirical and were developed for conventional polymer-salt
 191 ATPS, the results of our study reveal that they belong to the region of values (D, E) that
 192 describe the binodal curve of ILATPS with the highest accuracy when this equation is
 193 used.
 194



195
 196 Fig. 2-Fitting of the mean R^2 to the quadratic polynomial function depending on the
 197 values of Merchuk's equation exponents.
 198

199 3.2. Development and assessment of alternative binodal curve models for ILATPS

200 Different models were developed and their performance when describing the binodal
 201 curve of ILATPS was assessed. Table 2 summarizes the different alternative versions of
 202 the Merchuk's equation tested, considering models with a different number of total
 203 parameters and adjusted parameters, and also models explicit in both variables (i.e. [IL],
 204 concentration of IL and [S], concentration of salt) or not. The mean values of statistical
 205 criteria R^2 , F, RSME and AIC obtained when each of these models was used for the

206 ILATPS of the database are reported in Table 3, together with the confidence intervals,
 207 for which the median values are reported due to the higher robustness to extreme values
 208 that can be obtained in some ILATPS, as previously mentioned.

209

210 Table 2-Models assessed to describe the binodal curve of ILATPS.

| Model No. | Model | No. of parameters | No. of adjusted parameters | Explicit in the two variables |
|-----------|---|-------------------|----------------------------|-------------------------------|
| 1 | $[IL] = A \cdot \exp(B[S]^D - C[S]^3)$ | 5 | 4 | NO |
| 2 | $[IL] = A \cdot \exp(B[S]^{0.5} - C[S]^E)$ | 5 | 4 | NO |
| 3 | $[IL] = A \cdot \exp(B[S]^{0.5} - C[S]^3)$ | 5 | 3 | NO |
| 4 | $[IL] = A \cdot \exp(B[S]^D)$ | 3 | 3 | YES |
| 5 | $[IL] = A \cdot \exp(B[S])$ | 2 | 2 | YES |
| 6 | $[IL] = \exp(a + b[S]^{0.5} + c[S] + d[S]^2)$ | 6 | 4 | NO |
| 7 | $\ln\left(V_{213}^* \frac{[S]}{M_S} + f_{213}\right) + V_{213}^* \frac{[IL]}{M_{IL}} = 0$ | 4 | 2 | YES |

211

212 Table 3-Summary of statistical criteria for the assessment of the models developed.
 213 Model numbers correspond to those listed in Table 2.

| Model No. | Mean R ² | Median confidence interval | Mean F | Mean RSME | Mean AIC |
|-----------|---------------------|----------------------------|--------------------|-----------|----------|
| 1 | 0.9991 | 27.50 % | $2.088 \cdot 10^5$ | 0.3264 | -137.4 |
| 2 | 0.9989 | 47.86 % | $1.704 \cdot 10^5$ | 0.3585 | -128.7 |
| 3 | 0.9981 | 5.728 % | $1.556 \cdot 10^5$ | 0.4469 | -108.4 |
| 4 | 0.9964 | 11.67 % | $5.559 \cdot 10^4$ | 0.6579 | -55.07 |
| 5 | 0.9900 | 2.694 % | $3.406 \cdot 10^4$ | 1.025 | -12.08 |
| 6 | 0.9992 | 22.01 % | $1.990 \cdot 10^5$ | 0.3188 | -137.4 |
| 7 | 0.9686 | 13.73 % | $2.035 \cdot 10^4$ | 1.646 | 41.56 |

214

215 As shown in Table 2, Models 1 and 2 included an additional adjusted parameter
 216 compared to the original Merchuk's equation (Model 3). Table 3 shows that both
 217 Models 1 and 2 gave very similar results, enhancing the accuracy with respect to the
 218 performance of the Merchuk's equation (e.g. mean RSME is reduced 27% in Model 1
 219 and 20% in Model 2 with respect to Model 3). Moreover, despite the lower median

220 confidence interval obtained with Model 3, which can be explained considering that it
221 contains only 3 adjustable parameters instead of 4, in most of the ILATPS assessed, the
222 values of the parameters of model 2 and, especially, of model 1 were statistically
223 significant, so the inclusion of the fourth parameter is advisable, which is also proved
224 by the AIC values. However, it should be mentioned that the 5-adjusted parameter
225 equation (not included in Tables 2 and 3) leads to overfitting, since most of the
226 parameters were not statistically significant. In addition, even though Models 1 and 2
227 only differ in the exponent that is adjusted, Model 1 clearly describes better the binodal
228 curve, so the use of Model 2 is discarded. It is also important to note that the
229 mathematical complexity of these models is identical, since all the parameters (fixed
230 and adjusted) are constant once their values have been obtained. Therefore, the use of
231 Model 1 is recommended when the maximum accuracy of the binodal curve is required.
232 All the previous models (1-3) are implicit in the salt concentration. For this reason,
233 other models that can be explicit in the two variables ([IL] and [S]) were also
234 developed, because, as already mentioned, reducing the mathematical complexity of the
235 equation for the binodal curve can be important when it is used in complex modeling
236 problems to make convergence easier. In this sense, Model 4 is outstanding, since it
237 contains 3 adjustable parameters and it is explicit in both variables (Table 2), providing
238 relatively high accuracy, with $R^2 > 0.996$ and $RMSE < 0.66$ (Table 3). Decreasing the
239 number of adjusted parameters to 2 (model 5, Table 2), the accuracy of the fitting is
240 considerably reduced, although maintaining an acceptable mean value of $R^2=0.990$.
241 More interestingly and as shown in Table 3, Model 5 shows the narrowest error range of
242 all models, which implies that the significance is increased. Nevertheless, in the other
243 cases, when explicit models in the two variables are more suitable, Model 4 is

244 recommended due to its higher accuracy, which is not very different from that obtained
245 with the original Merchuk's equation (Model 3).

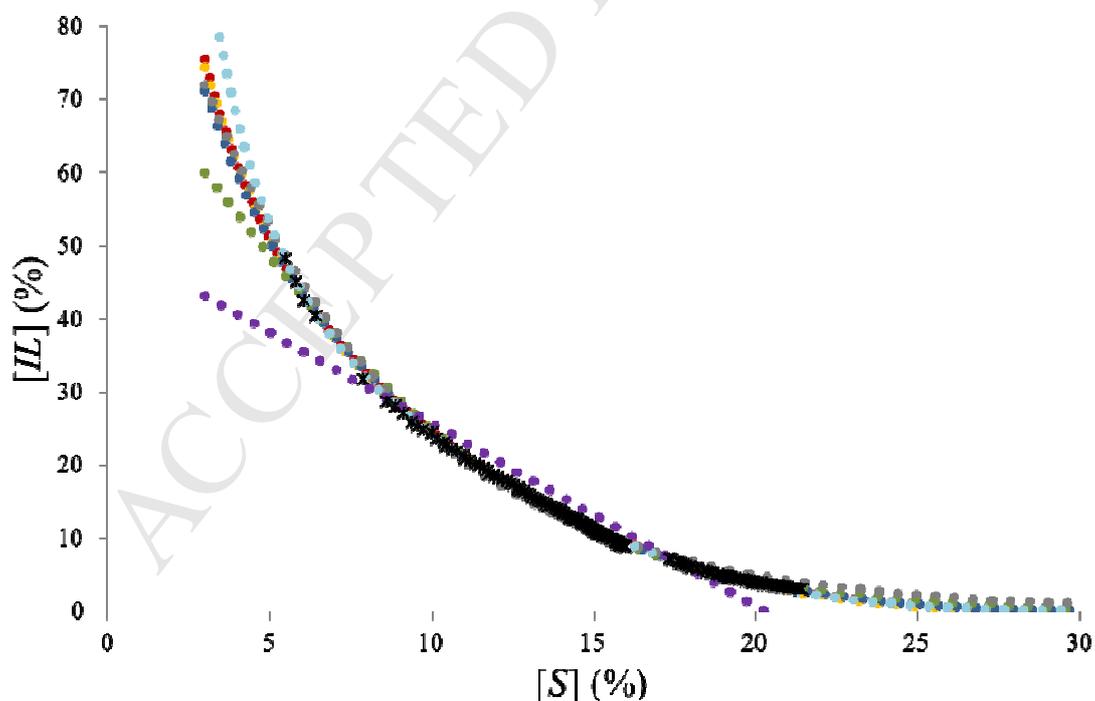
246 Other models, previously reported in literature and following distinct approaches from
247 the Merchuk's equation, were also analyzed in this work. Model 6 is another empirical
248 model with 6 parameters (considering both fixed and adjusted), while Model 7 is the
249 theoretical model originally developed for aqueous polymer-polymer systems but that
250 has been proposed to be used also for ILATPS [15,17-19]. It should be mentioned that
251 tests with the model of Eq. 3 were also carried out, although the results are not shown
252 because it suffered from computational problems and, in the cases where it was possible
253 to obtain adjusted parameters, most of them were not significant.

254 It can be seen in Table 3 that Model 6 leads to a goodness of fit almost identical to that
255 provided by Model 1, but it contains an additional fixed parameter. Furthermore,
256 considering that Merchuk's equation is more widely used than Model 6, the replacement
257 of Model 1 by Model 6 is not recommended. On the other hand, Model 7 clearly shows
258 the poorest results among all the models analyzed. Even though Models 5 and 7 contain
259 the same number of adjustable parameters and Model 7 has two additional fixed
260 parameters, Model 5 clearly describes the binodal data of ILATPS more accurately. In
261 addition, it should be noted that the parameter significance of models 3 and 4 is higher
262 than the significance of model 7, since the latter leads to a wider median confidence
263 interval even though it implies one adjusted parameter less. This confirms that the use
264 of model 7 is not advisable to describe the binodal curve of ILATPS. Therefore, these
265 results reveal that the approaches such as Model 7 based on the calculation of the
266 effective excluded volume (EEV), which were developed for aqueous polymer-polymer
267 systems, cannot describe adequately the binodal curve of ILATPS because the

268 assumptions involved in this theory [15,17-19] cannot be extended to ionic
269 liquid/salt/water systems.

270 Finally, in order to exemplify how each model describes the binodal data and
271 extrapolates the binodal curve to a wider range of compositions, Figure 3 shows the
272 experimental binodal data and the binodal curve simulated by each model of the
273 ILATPS formed by $[P_{i(444)1}][Tos]$ as ionic liquid and K_2HPO_4/KH_2PO_4 as the salt
274 component (system number 58, see Supplementary material). As can be seen, Models 1-
275 6 lead to a similar fitting of the binodal data, which is in accordance with the relatively
276 high accuracy achieved by all of them ($R^2 \geq 0.99$, $AIC < 0 \dots$). However, it is clear that
277 Model 7 cannot describe the trend of the binodal data, which reinforces the idea that this
278 model is not suitable for ILATPS. Regarding the values of the parameters, clear trends
279 have not been detected, although this work is not focused on predictive purposes.

280



281

282 Figure 3-Binodal data of the ILTAPS formed by $[P_{i(444)1}][Tos]$ as ionic liquid and
283 K_2HPO_4/KH_2PO_4 as the salt component (system number 58, see Supplementary

284 material). Notation: experimental data (*); simulated data by: Model 1 (●), Model 2
 285 (●), Model 3 (●), Model 4 (●), Model 5 (●), Model 6 (●) and Model 7 (●).

286

287 **3.3. Improving the accuracy at high salt mass fractions: alternative fitting method**

288 For the analysis of the recyclability of the IL in separation processes based on ILATPS,
 289 the IL present in the salt-rich phase is critical since it may constitute the losses of the
 290 process. Therefore, the correct assessment of the IL concentration in this phase is
 291 critical, which corresponds to the region of the binodal curve at high salt concentrations
 292 [12,13]. However, in this region, even low absolute errors in a binodal curve model may
 293 imply high relative errors when determining the mentioned concentration of IL.

294 As usual, in the models already discussed in previous analyses, the method of least
 295 squares based on the minimization of the sum of absolute errors, S , was used for fitting

296 the data: $Min S = \sum_{i=1}^n (y_i - \hat{y}_i)^2$, where y_i and \hat{y}_i are the observed and fitted response

297 values, respectively. In this case, the observed values correspond to the concentration of
 298 ionic liquid for a given salt concentration that defines the biphasic region in the phase
 299 diagram. Nevertheless, in this section, with the aim of improving the performance of the
 300 models at high salt mass fractions, the results obtained using an alternative method for
 301 fitting the binodal curve based on minimizing the sum of the relative errors (instead of

302 the sum of the absolute errors) is presented: $Min S = \sum_{i=1}^n \frac{|y_i - \hat{y}_i|}{y_i}$. It should be noted

303 that the relative errors will always be positive, since, in this case, y_i is the experimental
 304 mass fraction of ionic liquid for a given salt concentration i , which is an intrinsically
 305 positive variable.

306

307

308 Table 4-Comparison of the results using two alternative fitting methods: method of least
 309 squares based on minimization of absolute errors (called “least squares” in the table);
 310 and fitting method based on minimization of relative errors (“relative error”). Model
 311 numbers correspond to those listed in Table 2.

| Model No. | Mean relative error in absolute value (%) | | | | Mean RSME | |
|-----------|---|----------------|-------------------------------|----------------|---------------|----------------|
| | All binodal curve | | 5 points with the lowest [IL] | | Least squares | Relative error |
| | Least squares | Relative error | Least squares | Relative error | | |
| 1 | 1.055 | 0.8983 | 2.334 | 1.453 | 0.3264 | 0.3775 |
| 3 | 1.498 | 1.135 | 3.724 | 1.964 | 0.4469 | 0.6254 |
| 4 | 2.633 | 1.726 | 7.000 | 2.946 | 0.6579 | 0.9975 |
| 5 | 4.530 | 3.414 | 11.96 | 6.824 | 1.025 | 1.676 |

312

313 The comparison of the results obtained using different models that were fitted with the
 314 two methods is reported in Table 4, in which the mean relative errors in absolute value
 315 have been calculated according to Equation 5:

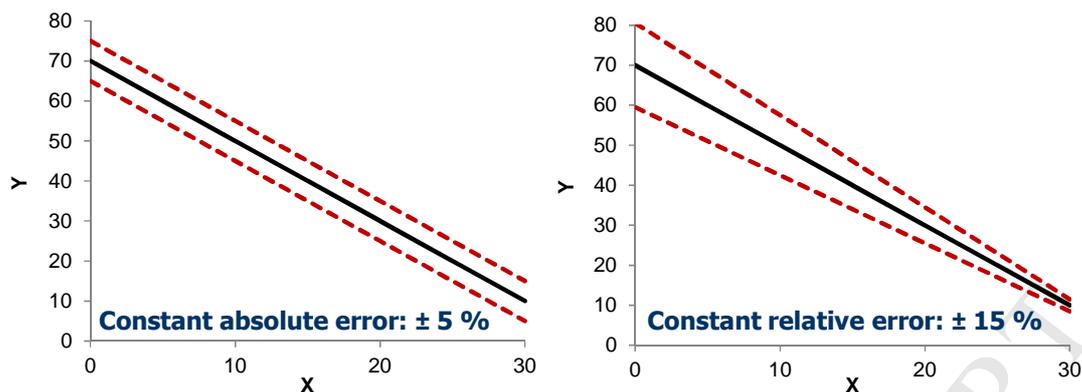
$$316 \text{ Mean relative error in absolute value (\%)} = 100 \frac{\sum_{j=1}^n \frac{\sum_{i=1}^{n_j} |y_{i,j} - \hat{y}_{i,j}|}{n_j}}{n} \quad (5)$$

317 where j denotes the different ILATPS included in the database and i represents each
 318 binodal data of the ILTAPS j , so n_j is the available number of experimental points of the
 319 binodal curve of j , and n is the number of ILAPTS (in this particular study $n=100$). The
 320 models chosen for comparison are those identified as the most suitable ones to model
 321 the binodal curve, including both non explicit (Models 1 and 3) and explicit (Models 4
 322 and 5). The results summarized in Table 4 show that the fitting methods based on the
 323 minimization of the relative errors reduced the mean relative errors between 15 % (in
 324 Model 1) and 34 % (in Model 4) with respect to the least squares method, keeping the
 325 mean RSME in relatively low values, which were lower than 1 for Models 1, 3 and 4.

326 It is particularly interesting to focus on analyzing the performance of the models with
 327 both fitting methods when dealing with the part of the binodal curve with the lowest

328 concentration of IL, since this is the most important region of the curve to assess the
329 recyclability of the IL. As can be seen in Table 4, for the 5 points of the binodal curve
330 with the lowest concentration of IL, the models developed using the fitting method
331 based on relative errors increased the reduction of the error to the range between 38 and
332 58 % compared to the corresponding models fitted with least squares. This behavior can
333 be explained considering that the least squares method tends to minimize absolute
334 errors, whereas the alternative fitting method proposed is based on the minimization of
335 relative errors. For this reason, assuming that in both cases the corresponding fitting
336 errors are kept constant along the binodal curve, even high relative errors (15 %) may
337 correspond to considerably lower absolute errors than a given low absolute error at low
338 values of the function (i.e., the region at high salt concentration), as graphically
339 exemplified in Fig. 4. This figure shows two generic independent and dependent
340 variables (X and Y, respectively), and demonstrates how the minimization of relative
341 errors reduces considerably the absolute error in the region of low values of Y,
342 increasing the error at high Y. In the case of binodal curves, the region of low Y
343 correspond to high salt mass fractions, *i.e.* the zone of the binodal curve identified as
344 crucial when looking for the ionic liquid recyclability. In this way, this alternative
345 fitting method clearly improves the accuracy of the models in this important region of
346 the binodal curve but without suffering from excessive errors in others, since the
347 absolute errors measured by means of RSME remain relatively low.

348



349

350 Fig. 4-Distribution of the fitting error at constant absolute (left) or relative (right) errors.
351

352 Therefore, these results reveal that the development of the models with a fitting method
353 that minimizes the relative errors instead of the absolute errors allowed enhancing the
354 accuracy of the fitting of the binodal curve of ILATPS in the most important region for
355 carrying out the ionic liquid recyclability analyses.

356

357 4. CONCLUSIONS

358 This work provides a critical assessment of the models of binodal curves of ILATPS,
359 and particularly, of the equation proposed by Merchuk and collaborators [10], since it is
360 the most widely applied. The results of this study confirm that even though the
361 empirical values of the exponents of Merchuk's equation (0.5 and 3.0) were developed
362 for polymer-salt ATPS, they are also valid for ILATPS, fitting the binodal curve with
363 the highest accuracy.

364 Alternative models have been proposed in this work to replace this equation with the
365 aim of increasing the accuracy or reducing the mathematical complexity, depending on
366 the requirements of each specific application. In this way, when accuracy is critical and
367 the binodal curve equation is not involved in complex models (i.e. convergence
368 problems are not expected), the proposed equation to describe this equilibrium curve

369 turns the first exponent of the Merchuk's equation into an adjusted parameter, D :

$$370 \quad [IL] = A \cdot \exp(B[S]^D - C[S]^3) .$$

371 However, the most complex models may suffer from convergence problems (e.g. large
372 non-linear optimization problems), so in these cases the binodal curve of ILATPS
373 should be explicit in the two variables so that iterative procedures are not required to
374 solve this clearly non-linear equation. For this purpose, the use of the following model
375 that contains 3 adjustable parameters and it is explicit in both the concentration of IL
376 and the concentration of salt, keeping relatively high accuracy ($R^2 > 0.996$ and $RMSE <$
377 0.66), is proposed: $[IL] = A \cdot \exp(B[S]^D)$.

378 Finally, a detailed study is carried out for the binodal curve at high salt concentrations,
379 due to the importance of this region for the recovery of the ionic liquid used in the
380 processes based on ILATPS. In this sense, the fitting method based on the minimization
381 of relative errors is recommended to increase significantly the accuracy of the binodal
382 curve in this crucial region for assessing the recyclability of the IL.

383

384 **Acknowledgements**

385 This work was developed in the scope of the project CICECO-Aveiro Institute of
386 Materials (Ref. FCT UID/CTM/50011/2013), financed by national funds through the
387 FCT/MEC and co-financed by FEDER under the PT2020 Partnership Agreement. The
388 authors also acknowledge FCT for the Post-doctoral grant SFRH/BPD/79263/2011 of
389 S.P.M. Ventura.

390

391

392 **REFERENCES**

393

- 394 [1] C.M.S.S. Neves, S.P.M. Ventura, M.G. Freire, I.M. Marrucho, J.A.P. Coutinho,
395 Evaluation of Cation Influence on the Formation and Extraction Capability of
396 Ionic-Liquid-Based Aqueous Biphasic Systems, *J. Phys. Chem. B*, 113 (2009)
397 5194-5199.
- 398 [2] M.G. Freire, A.F.M. Cláudio, J.M.M. Araújo, J.A.P. Coutinho, I.M. Marrucho,
399 J.N.C. Lopes, L.P.N. Rebelo, Aqueous biphasic systems: a boost brought about by
400 using ionic liquids, *Chem. Soc. Rev.*, 41 (2012) 4966-4995.
- 401 [3] J.F.B. Pereira, S.P.M. Ventura, F.A. E Silva, S. Shahriari, M.G. Freire, J.A.P.
402 Coutinho, Aqueous biphasic systems composed of ionic liquids and polymers: a
403 platform for the purification of biomolecules, *Sep. Purif. Technol.* 113 (2013) 83-
404 89.
- 405 [4] E. Alvarez-Guerra, A. Irabien, Separation of Proteins by Ionic Liquid-Based
406 Three-Phase Partitioning, in: A. Perez de los Rios, F.J. Hernandez-Fernandez
407 (Eds.), *Ionic Liquids in Separation Technology*, Elsevier, Amsterdam, 2014, pp.
408 207-234.
- 409 [5] M. Domínguez-Pérez, L.I.N. Tomé, M.G. Freire, I.M. Marrucho, O. Cabeza,
410 J.A.P. Coutinho, (Extraction of biomolecules using) aqueous biphasic systems
411 formed by ionic liquids and aminoacids, *Sep. Purif. Technol.* 72 (2010) 85-91.
- 412 [6] S.P.M. Ventura, R.L.F. de Barros, J. M. de Pinho Barbosa, C.M.F. Soares, A.S.
413 Lima, J.A.P. Coutinho, Production and Purification of an Extracellular Lipolytic
414 Enzyme using Ionic Liquid-based Aqueous Two-phase Systems, *Green Chem.* 14
415 (2012) 734-740.
- 416 [7] M.V. Quental, H. Passos, K.A. Kurnia, J.A.P. Coutinho, M.G. Freire, Aqueous
417 Biphasic Systems Composed of Ionic Liquids and Acetate-Based Salts: Phase
418 Diagrams, Densities, and Viscosities, *J. Chem. Eng. Data* 60 (2015) 1674-1682.

- 419 [8] C.F.C. Marques, T. Mourão, C.M.S.S. Neves, A.S. Lima, I. Boal-Palheiros, J.A.P.
420 Coutinho, M.G. Freire, Aqueous Biphasic Systems Composed of Ionic Liquids
421 and Sodium Carbonate as Enhanced Routes for the Extraction of Tetracycline,
422 *Biotechnol. Prog.*, 29 (2013) 645-645.
- 423 [9] S. Shahriari, C.M.S.S. Neves, M.G. Freire, J.A.P. Coutinho, Role of the
424 Hofmeister Series in the Formation of Ionic-Liquid-Based Aqueous Biphasic
425 Systems, *J. Phys. Chem. B*, 116 (2012) 7252-7258.
- 426 [10] J.C. Merchuk, B.A. Andrews, J.A. Asenjo, Aqueous two-phase systems for
427 protein separation studies on phase inversion, *J. Chromatogr. B* 711 (1998) 285-
428 293.
- 429 [11] C.M.S.S. Neves, M.G. Freire, J.A.P. Coutinho, Improved recovery of ionic liquids
430 from contaminated aqueous streams using aluminium-based salts, *RSC Adv.* 2
431 (2012) 10882–10890.
- 432 [12] E. Alvarez-Guerra, S.P.M. Ventura, J.A.P. Coutinho, A. Irabien, Ionic Liquid-
433 based three phase partitioning (ILTPP) systems: Ionic liquid recovery and
434 recycling, *Fluid Phase Equilibr.* 371 (2014) 67-74.
- 435 [13] E. Alvarez-Guerra, S.P.M. Ventura, J.A.P. Coutinho, A. Irabien, Ionic Liquid
436 Recovery Alternatives in Ionic Liquid-Based Three Phase Partitioning (ILTPP),
437 *AIChE J.* 60 (2014) 3577-3586.
- 438 [14] E. Alvarez-Guerra, A. Irabien, Optimization of ionic liquid recycling in Ionic
439 Liquid-based Three Phase Partitioning processes, in: K.V. Gernaey, J.K. Huusom,
440 R. Gani (Eds.), *Computer-Aided Chemical Engineering*, 37, Elsevier, Amsterdam,
441 2015, pp. 1475-1480.
- 442 [15] Y. Li, M. Zhang, J. Wu, J. Shi, C. Shen, Liquid-liquid equilibria of ionic liquid N-
443 butylpyridinium tetrafluoroborate and disodium hydrogen phosphate/sodium

- 444 chloride/sodium sulfate/ammonium sulfate aqueous two-phase systems at
445 $T=298.15$ K: Experiment and correlation, *Fluid Phase Equilibr.* 378 (2014) 44-50.
- 446 [16] W. Zhang, G. Zhang, J. Han, Y. Yan, B. Chen, C. Sheng, Y. Liu, Phase
447 equilibrium and chloroamphenicol partitioning in aqueous two-phase system
448 composed of 1-hydroxylhexyl-3-methylimidazolium chloride-salt, *J. Mol. Liq.*
449 193 (2014) 226-231.
- 450 [17] Y. Li, L. Yang, X. Zhao, W. Guan, Liquid-liquid equilibria of ionic liquid N-
451 ethylpyridinium tetrafluoroborate + trisodium citrate/ammonium citrate
452 tribasic/sodium succinate/sodium tartrate aqueous two-phase systems at 298.15 K,
453 *Thermochim. Acta* 550 (2012) 5-12.
- 454 [18] I. Regupathi, S.L. Monteiro, 1-Hexyl-3-Methylimidazolium Chloride – Potassium
455 Carbonate Aqueous Two Phase System: Equilibrium Characteristics and BSA
456 Partitioning Behavior, *J. Disper. Sci. Technol.* 35 (2014) 418-427.
- 457 [19] J. Han, C. Yu, Y. Wang, X. Xie, Y. Yan, G. Yin, W. Guan, Liquid-liquid
458 equilibria of ionic liquid 1-butyl-3-methylimidazolium tetrafluoroborate and
459 sodium citrate/tartrate/acetate aqueous two-phase systems at 298.15 K:
460 Experiment and correlation, *Fluid Phase Equilibr.* 295 (2010) 98-103.
- 461 [20] Y. Guan, T.H. Lilley, T.E. Treffry, A new excluded volume theory and its
462 application to the coexistence curves of aqueous polymer two-phase systems,
463 *Macromolecules* 26 (1993) 3971–3979.
- 464 [21] G. Torres-Plasencia, E. Gutiérrez-Arnillas, F.J. Deive, M.A. Sanromán, A.
465 Rodríguez, Triggering phase disengagement of 1-alkyl-3-methylimidazolium
466 chloride ionic liquid by using inorganic and organic salts, *J. Chem.*
467 *Thermodynamics* 88 (2015) 1-7.

- 468 [22] H. Passos, A.R. Ferreira, A.F.M. Cláudio, J.A.P. Coutinho, M.G. Freire,
469 Characterization of Aqueous Biphasic Systems Composed of Ionic Liquids and a
470 Citrate-based Biodegradable Salt, *Biochem. Eng. J.* 67 (2012) 68–76.
- 471 [23] H. Passos, M.P. Trindade, T.S.M. Vaz, L.P. da Costa, M.G. Freire, J.A.P.
472 Coutinho, The Impact of Self-aggregation on the Extraction of Biomolecules in
473 Ionic-liquid-based Aqueous Two-phase Systems, *Sep. Purif. Technol.* 108 (2013)
474 174–180.
- 475 [24] T.B.V. Dinis, H. Passos, D.L.D. Lima, V.I. Esteves, J.A.P. Coutinho, M.G. Freire,
476 One-step Extraction and Concentration of Estrogens for an Adequate Monitoring
477 of Wastewaters Using Ionic-Liquid-Based Aqueous Biphasic Systems, *Green*
478 *Chem.* 17 (2015) 2570–2579.
- 479 [25] F.A. e Silva, T. Sintra, S.P.M. Ventura, J.A.P. Coutinho, Recovery of paracetamol
480 from pharmaceutical wastes, *Sep. Purif. Technol.* 122 (2014) 315–322.
- 481 [26] T.E. Sintra, R. Cruz, S.P.M. Ventura, J.A.P. Coutinho, Phase diagrams of ionic
482 liquids-based aqueous biphasic systems as a platform for extraction processes, *J.*
483 *Chem. Thermodyn.* 77 (2014) 206–213.
- 484 [27] S.P.M. Ventura, S.G. Sousa, L.S. Serafim, A.S. Lima, M.G. Freire, J.A.P.
485 Coutinho, Ionic Liquid Based Aqueous Biphasic Systems with Controlled pH:
486 The Ionic Liquid Cation Effect, *J. Chem. Eng. Data* 56 (2011) 4253–4260.
- 487 [28] S.P.M. Ventura, S.G. Sousa, L.S. Serafim, A.S. Lima, M.G. Freire, J.A.P.
488 Coutinho, Ionic Liquid Based Aqueous Biphasic Systems with Controlled pH:
489 The Ionic Liquid Anion Effect, *J. Chem. Eng. Data* 57 (2012) 507–512.
- 490 [29] M. Taha, M.R. Almeida, F.A. e Silva, P. Domingues, S.P.M. Ventura, J.A.P.
491 Coutinho, M.G. Freire, Novel Biocompatible and Self-buffering Ionic Liquids for
492 Biopharmaceutical Applications, *Chem. Eur. J.* 21 (2015) 4781–4788..

- 493 [30] M. Taha, F.A. e Silva, M.V. Quental, S.P.M. Ventura, M.G Freire, J.A.P.
494 Coutinho, Good's buffers as a basis for developing self-buffering and
495 biocompatible ionic liquids for biological research, Green Chem. 16 (2014) 3149-
496 3159.
- 497 [31] J. Esteban, E. Fuente, A. Blanco, M. Ladero, F. Garcia-Ochoa, Phenomenological
498 kinetic model of the synthesis of glycerol carbonate assisted by focused beam
499 reflectance measurements, Chem. Eng. J. 260 (2015) 434-443.